

Supporting Information

“Specific Solvation Interactions of CO₂ on Acetate and Trifluoroacetate Imidazolium Based Ionic Liquids at High Pressures”

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Results and Discussion

The results of the application of the thermodynamic consistency test to the binary systems containing ionic liquid is presented in Table 1. In this Table, NP is the number of data points, T is the temperature, k_{12} , α_{12} , g_{12} - g_{22} and g_{21} - g_{11} are the interaction parameters of the model, where 1 stands for the CO_2 and 2 for the ionic liquid. This Table is divided in sections for each system studied. The $\text{CO}_2 + [\text{C}_4\text{mim}][\text{Ac}]$ system determined by Shifflet et al.¹ was also investigated.

Thermodynamic Modeling and Consistency

Valderrama and Álvarez² developed a thermodynamic consistency test for systems with incomplete PT_{xy} data, cataloging them as thermodynamic consistent (TC), thermodynamic inconsistent (TI) or not full consistent (NFC). The authors analyzed the difficulties normally found when modeling this type of mixtures and proposed a methodology to analyze the experimental data, concluding about their thermodynamic consistency or inconsistency. Recently, Álvarez and Aznar^{3,4} applied an extension of this approach to several supercritical fluid + IL systems using a method based on the Gibbs-Duhem equation, on the fundamental phase equilibrium equation, and on the Peng-Robinson equation of state⁵, with the Wong-Sandler mixing rule⁶ using the UNIQUAC model⁷ for the activity coefficient. The NRTL (three adjustable parameters) and UNIQUAC (two adjustable parameters) models produce similar fit results, nonetheless the NRTL model is preferable when the data present a statistical quirk, caused by inaccurate measurements, as shown in Álvarez and Aznar publication.³ Therefore, the NRTL model was selected in the present work.

Similar to Van Ness-Byer-Gibbs test modeling procedure⁸, a thermodynamic model is used to accurately fit the experimental data and thereafter, apply the consistency test. The experimental data fit requires the calculation of several model parameters, using an optimized objective function. Although

the consistency test is model dependent, good fitting does not guarantee that the data are consistent, since the proposed area test, consequent from the Gibbs–Duhem equation, must also be fulfilled.

As described previously⁹, the test uses the Gibbs-Duhem equation expressed in the integral form, where the left-hand side is denoted as A_P and the right-hand side as A_ϕ , as it follows:

$$A_P = \int \frac{1}{Py_2} dp \quad (1)$$

$$A_\phi = \int \frac{(1-y_2)}{y_2(Z-1)} \frac{d\phi_1}{\phi_1} + \int \frac{1}{(Z-1)} \frac{d\phi_2}{\phi_2} \quad (2)$$

The values for A_P are obtained with experimental Py_2 data, and the values for A_ϕ are obtained with calculated values of Z , ϕ_i and y_2 . The subscripts 1 and 2 denote CO₂ and ionic liquid compounds, respectively. The individual percent area deviation, $\% \Delta A_i$, is given as:

$$\% \Delta A_i = 100 \left[(A_\phi - A_P) / A_P \right]_i \quad (3)$$

where the subscript i refer to the i^{th} data point. The quality of the correlation was analyzed through the relative deviations in the calculated pressure in the gas phase for each point i , defined as:

$$\% \Delta p_i = 100 (p_i^{\text{cal}} - p_i^{\text{exp}}) / p_i^{\text{exp}} \quad (4)$$

The method implies the minimization of the deviations of Eqs. 3 and 4 setting as the objective function, OF , for the consistency test the minimization of the deviations in VLE data and the individual percent area deviation.

$$OF = \sum_{i=1}^{N-1} \left[\frac{A_P - A_\phi}{\sigma_A} \right]_i^2 + \sum_{i=1}^N \left[\frac{p^{\text{cal}} - p^{\text{exp}}}{\sigma_P} \right]_i^2 + \sum_{i=1}^N \left[\frac{y_{\text{fluid}}^{\text{cal}} - 1}{\sigma_y} \right]_i^2 \quad (5)$$

where N is the number of data points, p is the pressure, y_{fluid} is the vapor mole fraction of the supercritical fluid for data point i , the superscripts “exp” and “cal” refers to the experimental and calculated values respectively, and σ_A , σ_P and σ_y are the standard deviations of those quantities. The experimental uncertainties in the pressure data were used for σ_P , the value 10^{-4} for σ_y and the value of

A_p for σ_A . The minimization method was performed using a genetic algorithm code, implemented and fully explained in Alvarez et al.¹⁰ The difference between experimental and calculated values was calculated as the average percent deviation, expressed in absolute form, as follows:

$$\%|\Delta p| = \frac{100}{N} \sum_{i=1}^N \left[|p_i^{cal} - p_i^{exp}| / p_i^{exp} \right] \quad (6)$$

The data set is considered consistent when the individual area deviation, $\% \Delta A_i$, is within acceptable defined deviations. The difference between experimental and calculated individual area is calculated as the average percent deviation, expressed in absolute form, as follows:

$$\%|\Delta A| = \frac{100}{N} \left[|A_\varphi - A_p| / A_p \right] \quad (7)$$

The isopleths, for the $\text{CO}_2 + [\text{C}_4\text{mim}][\text{Ac}]$ system and for the $\text{CO}_2 + [\text{C}_4\text{mim}][\text{TFA}]$ system, were interpolated with the method proposed by Álvarez and Aznar⁴ and the results are reported in supporting information.

The isopleths were interpolated with the method proposed by Álvarez and Aznar⁴ and the results are shown in Table 2, for the $\text{CO}_2 + [\text{C}_4\text{mim}][\text{Ac}]$ system and for the $\text{CO}_2 + [\text{C}_4\text{mim}][\text{TFA}]$ system, respectively.

Detailed results are shown in Tables 3 through 6. The tables are divided in two parts, the upper part shows the original data set, while the lower part shows the remaining data after removing some experimental points, that have been found to be thermodynamically inconsistent. Tables 3 and 5, show detailed results for the $\text{CO}_2 + [\text{C}_4\text{mim}][\text{Ac}]$ systems at 323.1 and 348.1 K from Shifflet et al.¹ In Table 3 some data present deviations out the established limit for $\% \Delta A_i$ (bold and italic type). Nonetheless, deviations within the established limits are obtained by eliminating those points.

The data for the $\text{CO}_2 + [\text{C}_4\text{mim}][\text{Ac}]$ system at 348.1 K from Shifflet et al.¹ presented in Table 5 presents deviations out the established limit for the values of $\% \Delta p_i$ and thereafter, the test could not be applied. In addition, the data from this work, at the same temperature, was correlated with confidence,

showing that the present data are more reliable. In Table 6, detailed results for the system CO₂ + [C₄mim][Ac] at 348 K show that, for the upper part, some data have deviations outside the established limits, in the final values of % ΔA_i (bold and italic type), while for the lower part, when two points from the original data set are eliminated (the two with the highest area deviation, highlighted in the upper part), the deviations for the remaining eight points are within the defined limits of -20% to +20%. Therefore, while the original set with nine data points is not fully consistent the new set with the remaining eight points is thermodynamically consistent.

The same procedure is applied for the data in Table 7 where detailed results for the system CO₂ + [C₄mim][TFA] at 298 K are presented. The original data are not fully consistent, but after removing one data point, the remaining eight points are within the defined limits of -20% to +20%, which are thermodynamically consistent.

The results obtained for the CO₂ + [C₄mim][Ac] system denote greater deviations for the $x_1 > 0.5$ isopleths, while the system CO₂ + [C₄mim][TFA] present greater deviations for the $x_1 > 0.65$ isopleths leading to not fully consistent isotherms.

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Table 1. Results of the consistency test for all the experimental data.

Reference	NP	T/K	k_{ij}	α_{12}	$g_{12}-g_{22}$ kJ/kmol	$g_{21}-g_{11}$ kJ/kmol	$ \Delta p $ %	$ \Delta A $ %	Result
CO ₂ + [C ₄ mim][Ac]									
1	5	283.10	1.0000	0.2000	-11249.9893	-1933.5936	25.3	19.7	-
	9	298.10	-0.3274	0.2341	-28123.0098	6021.4521	12.2	13.8	NFC
	9	323.10	1.0000	0.3171	-11198.7109	3059.0808	10.4	14.6	NFC
	9	348.10	1.0000	0.3531	-9138.5596	24552.2227	14.1	17.2	-
[This work]	6	313.10	-0.3284	0.2397	-40690.6016	17402.3555	1.6	19.7	NFC
	9	323.09	-0.3667	0.2469	-50782.2500	-1592.4650	1.5	23.5	NFC
	8	333.00	-0.4688	0.2635	-50449.5625	-1625.9657	1.0	13.1	NFC
	8	343.00	-0.4912	0.2876	-49008.6250	-1777.7466	1.5	15.2	NFC
	8	348.00	0.5083	0.3660	-39224.0273	-3483.0093	6.3	17.8	NFC
	8	352.98	-0.6875	0.2017	-88945.3125	-5754.0894	1.9	15.7	NFC
CO ₂ + [C ₄ mim][TFA]									
[This work]	7	294.00	0.2188	0.2002	33310.5703	-3054.2261	3.2	11.1	NFC
	7	298.00	0.2188	0.2000	34271.8711	-2903.0513	3.1	14.6	NFC
	7	303.00	0.2188	0.2000	35683.6055	-2633.8701	3.1	19.0	NFC
	7	313.00	0.2192	0.2000	37582.4805	-2372.4836	3.5	30.8	NFC
	7	323.00	0.2120	0.2000	39737.5508	-2080.5359	3.7	90.1	NFC
	6	333.00	0.9596	0.2462	89950.1328	52675.3438	16.5	11.5	NFC
	6	343.00	0.2020	0.2018	42681.1992	-1757.8231	5.6	47.4	NFC
	6	348.00	0.1959	0.2001	44655.1328	-1552.4625	5.5	57.8	NFC
	6	353.00	0.1973	0.2018	44912.1094	-1494.4839	5.6	71.6	NFC
	6	363.00	0.1759	0.2036	45757.1133	-1367.4760	9.9	10.2	NFC

Table 2. Interpolated VLE data for the system supercritical CO₂ (1) + [C₄mim][Ac] (2) and CO₂ (1) + [C₄mim][TFA] (2).

CO ₂ (1) + [C ₄ mim][Ac] (2)									
^{x₁} T(K)	0.201	0.251	0.300	0.351	0.402	0.450	0.500	0.55	0.6
313.10	-	0.496	1.403	2.593	4.108	5.731	-	-	67.371
323.09	0.228	0.845	1.908	3.383	5.213	7.403	13.515	34.649	75.526
333.00	0.380	1.245	2.502	4.247	6.509	9.527	18.058	41.557	-
343.00	0.617	1.705	3.195	5.243	8.038	12.142	22.900	47.955	-
348.00	0.779	1.956	3.576	5.799	8.892	13.627	25.417	50.946	-
352.98	0.975	2.220	3.980	6.400	9.806	15.224	27.988	53.863	-
CO ₂ (1) + [C ₄ mim][TFA] (2)									
^{x₁} T/K	0.225	0.300	0.401	0.502	0.601	0.650	0.679		
294.00	1.001	1.579	2.445	3.527	8.239	27.010	44.006		
298.00	1.139	1.771	2.723	3.956	10.406	29.326	46.545		
303.00	1.321	2.025	3.100	4.538	13.151	32.175	49.717		
313.00	1.709	2.586	3.940	5.856	18.452	37.715	56.063		
323.00	2.131	3.216	4.881	7.382	22.733	43.047	62.409		
333.00	2.588	3.915	5.906	9.117	28.216	48.169	-		
343.00	3.080	4.682	6.999	11.057	32.537	53.083	-		
348.00	3.338	5.092	7.566	12.102	34.400	55.462	-		
353.00	3.606	5.519	8.143	13.195	36.498	57.788	-		
363.00	4.166	6.425	9.320	15.521	42.004	62.284	-		

Table 3. Detailed results for CO₂ + [C₄mim][Ac] at 323.1 K from ¹.

$A_p \cdot 10^7$	$A_\phi \cdot 10^7$	$\% \Delta A_i$	p^{exp}	p^{cal}	$\% \Delta p$	y_1^{cal}	y_2^{cal}	x_1
(9 data points) $k_{ij} = 1.0000$, $\alpha_{12} = 0.3171$, $(g_{12}-g_{22}) = -11198.7109$, $(g_{21}-g_{11}) = 3059.0808$, $\Delta P (\%) = 10.4$								
0.0593	0.0957	61.50	0.010	0.003	-69.16	0.9999803	0.0000197	0.108
0.146	0.172	17.40	0.050	0.050	-0.01	0.9999992	0.0000008	0.176
1.22	1.16	-5.00	0.100	0.113	12.71	0.9999997	0.0000003	0.204
1.54	1.38	-10.10	0.400	0.420	5.23	0.9999999	0.0000001	0.263
1.78	1.75	-1.91	0.700	0.697	-0.48	1.0000000	0.0000000	0.292
2.07	2.07	0.10	1.000	0.987	-1.27	1.0000000	0.0000000	0.315
1.54	1.68	8.72	1.300	1.284	-1.25	1.0000000	0.0000000	0.334
4.56	5.13	12.50	1.500	1.499	-0.01	1.0000000	0.0000000	0.346
-	-	-	1.999	2.074	3.75	1.0000000	0.0000000	0.373
(7 data points) $k_{ij} = 1.0000$, $\alpha_{12} = 0.3244$, $(g_{12}-g_{22}) = -11206.7412$, $(g_{21}-g_{11}) = 2763.3943$, $\Delta P (\%) = 3.4$								
0.144	0.172	20.00	0.050	0.047	-6.28	0.9999992	0.0000008	0.176
1.23	1.19	-3.17	0.100	0.108	7.63	0.9999997	0.0000003	0.204
1.58	1.44	-8.80	0.400	0.411	2.99	0.9999999	0.0000001	0.263
1.85	1.83	-0.69	0.700	0.687	-1.89	1.0000000	0.0000000	0.292
2.16	2.18	1.19	1.000	0.978	-2.24	1.0000000	0.0000000	0.315
1.61	1.77	9.80	1.300	1.275	-1.94	1.0000000	0.0000000	0.334
-	-	-	1.500	1.491	-0.56	1.0000000	0.0000000	0.346

Table 4. Detailed results for CO₂ + [C₄mim][Ac] at 323.09 K from this work.

A_p	A_ϕ	$\% \Delta A_i$	p^{exp}	p^{cal}	$\% \Delta P$	y_1^{cal}	y_2^{cal}	x_1
(9 data points) $k_{ij} = 1.0000$, $\alpha_{12} = 0.3171$, $(g_{12}-g_{22}) = -11198.7109$, $(g_{21}-g_{11}) = 3059.0808$, $ \Delta P (\%) = 10.4$								
6.81E+13	6.87E+13	0.95	0.228	0.233	2.14	1.000000	0.000000	0.201
7.48E+13	7.15E+13	-4.35	0.845	0.873	3.31	1.000000	0.000000	0.251
4.01E+13	3.96E+13	-1.25	1.908	1.920	0.61	1.000000	0.000000	0.300
1.09E+13	1.11E+13	2.16	3.383	3.401	0.54	1.000000	0.000000	0.351
1.30E+12	1.42E+12	8.64	5.213	5.316	1.97	1.000000	0.000000	0.402
7.09E+10	6.11E+10	-13.80	7.403	7.793	5.27	1.000000	0.000000	0.450
9.10E+05	3.41E+05	-62.60	13.515	14.234	5.32	0.999999	0.0000009	0.500
6.21E+03	6.21E+03	0.00	34.649	32.819	-5.28	0.999897	0.0001027	0.550
-	-	-	75.526	66.592	-11.83	0.999418	0.0005825	0.599
(7 data points) $k_{ij} = -0.8433$, $\alpha_{12} = 0.2261$, $(g_{12}-g_{22}) = -55755.3516$, $(g_{21}-g_{11}) = -552.6208$, $ \Delta P (\%) = 4.0$								
2.97E+14	3.15E+14	6.20	0.228	0.223	-2.14	1.000000	0.000000	0.201
2.57E+14	2.51E+14	-2.55	0.845	0.882	4.37	1.000000	0.000000	0.251
8.45E+13	8.28E+13	-2.02	1.908	1.969	3.20	1.000000	0.000000	0.300
1.14E+13	1.13E+13	-1.47	3.383	3.482	2.93	1.000000	0.000000	0.351
5.61E+11	5.71E+11	1.77	5.213	5.374	3.09	1.000000	0.000000	0.402
9.56E+09	8.77E+09	-8.28	7.403	7.717	4.24	1.000000	0.000000	0.450
-	-	-	13.515	14.605	8.06	0.9998809	0.0001191	0.500

Table 5. Detailed results for CO₂ + [C₄mim][Ac] at 348.1 K from ¹.

A_p	A_ϕ	$\% \Delta A_i$	p^{exp}	p^{cal}	$\% \Delta P$	y_1^{cal}	y_2^{cal}	x_1
(9 data points) $k_{ij} = 1.0000$, $\alpha_{12} = 0.3531$, $(g_{12}-g_{22}) = -9138.5596$, $(g_{21}-g_{11}) = 24552.2227$, $ \Delta P (\%) = 14.2$								
			0.0104	0.0097	-6.69	0.9999002	0.0000998	0.063
			0.0505	0.0555	9.98	0.9999855	0.0000145	0.129
			0.1	0.1185	18.50	0.9999941	0.0000059	0.161
			0.4002	0.4206	5.10	0.9999988	0.0000012	0.226
			0.6994	0.6489	-7.21	0.9999993	0.0000007	0.253
			1.0003	0.8572	-14.30	0.9999995	0.0000005	0.272
			1.2994	1.0532	-18.95	0.9999996	0.0000004	0.287
			1.4997	1.1549	-22.99	0.9999997	0.0000003	0.294
			1.9993	1.5237	-23.79	0.9999998	0.0000002	0.316

Table 6. Detailed results for CO₂ + [C₄mim][Ac] at 348.0 K from this work.

A_p	A_ϕ	$\% \Delta A_i$	p^{exp}	p^{cal}	$\% \Delta P$	y_1^{cal}	y_2^{cal}	x_1
(8 data points) $k_{ij} = 0.5083$, $\alpha_{12} = 0.3660$, $(g_{12}-g_{22}) = -39224.0273$, $(g_{21}-g_{11}) = -3483.0093$, $ \Delta P (\%) = 6.3$								
1.59E+11	1.58E+11	-1.08	0.779	0.779	0.00	1.0000000	0.0000000	0.201
1.86E+11	1.86E+11	-0.11	1.956	1.939	-0.89	1.0000000	0.0000000	0.251
1.70E+11	1.72E+11	1.03	3.576	3.547	-0.81	1.0000000	0.0000000	0.300
1.05E+11	1.06E+11	0.14	5.799	5.800	0.01	1.0000000	0.0000000	0.351
3.47E+10	3.20E+10	-7.81	8.893	8.983	1.02	1.0000000	0.0000000	0.402
2.97E+09	1.54E+09	-48.10	13.627	13.804	1.30	1.0000000	0.0000000	0.450
2.52E+07	8.47E+06	-66.30	25.417	22.318	-12.19	1.0000000	0.0000000	0.500
-	-	-	50.946	33.341	-34.56	0.9999991	0.0000009	0.550
(6 data points) $k_{ij} = 0.7969$, $\alpha_{12} = 0.4229$, $(g_{12}-g_{22}) = -32920.5625$, $(g_{21}-g_{11}) = -3534.8833$, $ \Delta P (\%) = 1.2$								
2.76E+10	2.68E+10	-2.81	0.779	0.789	1.29	1.0000000	0.0000000	0.201
4.10E+10	4.08E+10	-0.61	1.956	1.930	-1.33	1.0000000	0.0000000	0.251
5.34E+10	5.44E+10	1.89	3.576	3.515	-1.72	1.0000000	0.0000000	0.300
5.26E+10	5.40E+10	2.49	5.799	5.754	-0.77	1.0000000	0.0000000	0.351
3.03E+10	2.85E+10	-5.94	8.893	8.955	0.70	1.0000000	0.0000000	0.402
-	-	-	13.627	13.800	1.27	1.0000000	0.0000000	0.450

Table 7. Detailed results for CO₂ + [C₄mim][TFA] at 298 K from this work.

A_p	A_ϕ	$\% \Delta A_i$	p^{exp}	p^{cal}	$\% \Delta P$	y_1^{cal}	y_2^{cal}	x_1
(7 data points) $k_{ij} = 0.2188$, $\alpha_{12} = 0.2000$, $(g_{12}-g_{22}) = 34271.8711$, $(g_{21}-g_{11}) = -2903.0513$, $ \Delta P (\%) = 3.1$								
3.08E+07	3.03E+07	-1.52	1.140	1.112	-2.4	1.0000000	0.0000000	0.225
2.94E+07	3.40E+07	15.6	1.771	1.718	-3.0	1.0000000	0.0000000	0.300
1.72E+07	2.07E+07	20.6	2.723	2.814	3.3	1.0000000	0.0000000	0.401
2.11E+07	1.84E+07	-12.8	3.956	4.386	10.9	1.0000000	0.0000000	0.502
2.20E+04	2.42E+04	10.3	10.406	10.274	-1.3	0.9999431	0.0000569	0.601
9.81E+03	1.24E+04	26.5	29.326	29.156	-0.6	0.9999461	0.0000539	0.650
-	-	-	46.545	46.501	-0.1	0.9999577	0.0000423	0.679
(5 data points) $k_{ij} = 0.2236$, $\alpha_{12} = 0.2059$, $(g_{12}-g_{22}) = 34037.5859$, $(g_{21}-g_{11}) = -2354.5664$, $ \Delta P (\%) = 6.2$								
3.04E+07	2.87E+07	-5.55	1.140	1.226	7.58	1.0000000	0.0000000	0.225
2.76E+07	3.04E+07	10.10	1.771	1.862	5.18	1.0000000	0.0000000	0.300
7.39E+07	7.18E+07	-2.93	2.723	2.985	9.61	1.0000000	0.0000000	0.401
2.30E+04	2.29E+04	-0.35	10.406	11.321	8.79	0.9999449	0.0000551	0.601
-	-	-	29.326	29.329	0.01	0.9999501	0.0000499	0.650